

# The fundamentals of the crack formation: chemistry and physics

*Gonzalo Alvarez de Toledo, Nora Egido Pérez Sidenor I+D 48970 Basauri. Bizkaia* 

SPAIN





SWERI/M

Ssidenor

RI A



B<sub>F</sub>i





### Introduction

## History of continuous casting at Sidenor

SWERIM	YEAR	CASTING	CASTING	STEEL	OBSERVATIONS
		SIZES (mm)	SPEED	GRADES	
Ssidenor	< 1985	125			Much knowledge developed
		145		More difficult	New technologies: EMS, mould and
	1985 – 2000	145		to cast	oscillation, secondary cooling
RIR		170	Continuous	Microalloyed steel	Advances on online control
	2000 - 2018	155	increase	grades: Al, N, V, B,	However:
Materials Processing		185		Nb	The productivity requirements,
	>2018	155		Microalloyed + S.	More difficult to cast steel grades
		185			Higher quality requirements.
BFI		240	•		CRACKING REMAINS A BIG PROBLEM
-	BLOOM > 2012	350x470			



### Introduction

#### **Internal defects:**

- 1. Off-corner cracks
- 2. Corner cracks
- SWERI/M

RIR

Materials Processing

B<sub>F</sub>i

- 3. Half-Way Crack
  - 4. Transversal cracks
  - 5. Star-Crack
- **Ssidenor** 6. Central pipe
  - 7. Pore, blown holes
  - 8. Powder entrapment

#### Surface defects:

- 9. Corner cracks
- 10. Longitudinal cracks
- 11. Thermal/transformation longitudinal cracks
- 12. Corner transversal cracks
- 13. Face transversal cracks
- 14. Intergranular cracks (corner)
- 15. Intergranular cracks (face)
- 16. Surface star cracks Start cracks
- 17. Pores, blow holes
- 18. Powder entrapment





### Introduction





Bellet, Michel, et al. Metallurgical and Materials Transactions A 40.11 (2009): 2705-2717. [Hunt, B. Stewart, 9th ECCC, European Continuous Casting Conference, 2017, p. 620

#### 5/03/2020

## Worshop on microalloyed steels and cracks in continuously cast billets



www.valcra.eu





#### AGENDA

**9:15 -9:30 h Introduction**. Classification of cracks in continuously cast billets. Objectives of the European dissemination Project VALCRA.

## 9:30 -10:45 h Internal segregation cracks (Ghost lines)

- Formation mechanism. Influence of S, Mn and Boron.
- Influence of casting parameters.

10.45 - 11.00 h Coffee break

#### 11:00 – 12:15 h Surface cracks in billets

- Influence of microalloyed elements on hot ductility: Ti, Al, B, Nb, V, N.
- Influence of casting conditions

## **12:15 - 12.45 h** Thermal/transformation cracking in the tertiary cooling.

12:45 - 13.00 h Final conclusions







# Sidenor

## **1. Introduction**

#### **Chemical composition**

#### SWERIM

Ssidenor

High temperature ductility troughs during solidification and cooling of the CC billet.

RIR

![](_page_9_Picture_8.jpeg)

B<sub>F</sub>i

LDZ I: Internal segregation cracking.
LDZ II and LDZIII: Surface Cracks and Thermal/transformation cracks

![](_page_9_Figure_10.jpeg)

![](_page_10_Picture_1.jpeg)

## **2. Internal segregation cracks**

#### SWERI/M

Ssidenor

RIR

Materials

B<sub>F</sub>i

- **1. Segregation cracking formation mechanism**
- 2. Influence of composition on segregation cracking: Sulfur, Boron
- 3. Classification of cracks: Half-way cracking, Off-corner cracking, Near corner cracking.

![](_page_11_Picture_1.jpeg)

## **2. Internal segregation cracks**

18NiCrMo5E 185 mm billet. Hot acid eching. Crystal columnar growth area. Distance to billet surface: 60 mm.

![](_page_11_Picture_4.jpeg)

Ssidenor

![](_page_11_Picture_6.jpeg)

![](_page_11_Picture_7.jpeg)

![](_page_11_Picture_8.jpeg)

![](_page_11_Picture_9.jpeg)

Strain to produce cracking: >0.5%

Composition susceptible to segregation cracking: low melting interdendritic liquid.

Chemical elements: C, S, B, Nb. Mn/S < (Mn/S)c $(Mn/S)c = 1,345 \cdot S^{(-0,7934)}$ 

![](_page_12_Picture_1.jpeg)

## 2. Internal segregation cracks

![](_page_12_Figure_3.jpeg)

RIR

Materials Processing

B<sub>F</sub>i

![](_page_12_Picture_4.jpeg)

Half-way cracks Secondary cooling

![](_page_12_Picture_6.jpeg)

![](_page_12_Picture_7.jpeg)

Off-corner cracks Mould lower part or exit of the mold

![](_page_12_Picture_9.jpeg)

![](_page_12_Picture_10.jpeg)

Near corner cracks Foot rolls or Zone 2. Two nozzles by billet face.

![](_page_13_Picture_1.jpeg)

## 3. Surface cracks on billets: intergranular and transversal cracking

#### SWERI/M

Ssidenor

RIR

**Materials** 

- 1. Introduction: stresses at the surface of the CCM
- 2. Influence of the  $\gamma/\alpha$  transformation and of the Austenitic Grain Size on cracking
- 3. Influence of the microalloying elements on hot ductility.
  - 4. Methods to avoid intergranular cracking: On-line double  $\gamma/\alpha$  transformation and secondary cooling influence.

![](_page_13_Picture_8.jpeg)

# Sidenor

## 3. Surface cracks on billets: intergranular and transversal cracking

SWERIM

Ssidenor

![](_page_14_Picture_5.jpeg)

![](_page_14_Picture_6.jpeg)

![](_page_14_Picture_7.jpeg)

Billet corner of sample S3B4, 19MnNbV5C steel grade. Hot acid etching

![](_page_14_Picture_9.jpeg)

![](_page_14_Picture_10.jpeg)

![](_page_15_Picture_1.jpeg)

## 2. Surface cracks on billets: intergranular and transversal cracking

![](_page_15_Figure_3.jpeg)

# Sidenor

## 3. Influence of the microalloying elements on hot ductility.

#### Influence of the AIN

SWERI/M

![](_page_16_Figure_5.jpeg)

![](_page_16_Picture_6.jpeg)

![](_page_16_Picture_7.jpeg)

B<sub>F</sub>i

![](_page_16_Figure_9.jpeg)

- Ductility curves of a C-Mn steel with a 0.050% of aluminum in composition and different N contents.
- As the product Al\*N increases, the ductility trough widens, this being related to AIN precipitating at higher temperatures.

![](_page_16_Figure_12.jpeg)

Relationship between crack index and the N\*Al product.

![](_page_17_Figure_0.jpeg)

![](_page_18_Picture_1.jpeg)

## 4. Transformation Stress Cracks at the tertiary cooling

#### **Transformation influence: Volume changes**

#### SWERIM

- Ssidenor
- RIR

![](_page_18_Picture_7.jpeg)

B<sub>F</sub>i

stamping, the volume expansion related with the γ/α transformation changes the shrinkage pattern.
Nevertheless, even for a 30

26 minutes after the

 Nevertheless, even for a so minutes time, untransformed inner billet continues to shrinks due to decreasing temperatures.

![](_page_18_Figure_10.jpeg)

![](_page_19_Picture_1.jpeg)

Casting time for

## **Transformation Stress Cracks at the tertiary cooling**

#### Example: 16MnCr5E

![](_page_19_Figure_4.jpeg)

![](_page_20_Picture_0.jpeg)

![](_page_20_Picture_1.jpeg)

![](_page_20_Picture_2.jpeg)

![](_page_20_Picture_3.jpeg)

B<sub>F</sub>i

![](_page_20_Picture_4.jpeg)

Materials Processing Institute Contact: gonzalo.alvarezdetoledo@sidenor.com nora.egido@sidenor.com

![](_page_20_Picture_7.jpeg)

![](_page_20_Picture_8.jpeg)